

# R142b、R152a 等64种工质的热力性质的计算

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**提 要** 在本世纪末即将全面禁止使用 CFCs。对于 R11 和 R12 的替代工质, 例如 R123 和 R134a 的热力性质已有很多文章发表。本文给出了计算工质热力性质必须的全部公式, 并编制了通用计算程序, 用来计算 R142b、R152a 等替代工质的热力性质, 所得结果与现有的工质性质图表所列数据吻合。

**关键词** CFCs, 替代工质, 热力性质

由于在全球范围内限期禁用 CFCs, 1991年6月19日在“关于破坏臭氧层的蒙特列尔议定书”缔约国第三次会议上我国正式宣布加入该项议定书。

目前除替代工质 R123、R134a 有较可靠的热力数据外, 对 R142b 和 R152a 工质尚缺乏完整的热力性质参数。

本文以文献为[Перельштейн, 1984]依据, 根据4个基本方程应用热力学一般关系式[陈德雄等, 1988]获得三个导出方程并编制了通用计算程序。给出了 R142b、R152a 等64种工质热力性质的计算公式和程序, 基准点及相关的积分常数。

## 1 计算公式

### 1.1 状态方程

$$\begin{aligned} \text{令 } \tau = T/T_{KP} \quad V_0 = RT_{KP}/P_{KP} \\ Z = PV/RT = 1 \times 10^{-2} + [(b_1 + b_2/\tau + b_3/\tau^3)(V_0/V) + (b_4 + b_5/\tau + b_6/\tau^3)(V_0/V)^2 \\ + (b_7/\tau^3)(V_0/V)^3] \times 10^{-5} \end{aligned}$$

### 1.2 比热方程

$$C_v^0 = d_0 + d_1\tau + d_2\tau^2 + d_3\tau^3 + d_4\tau^4$$

### 1.3 饱和蒸汽压方程

$$P = P_{KP} \text{EXP}[(R_i \ln \tau + (R_i - 4 + P_s)(C_1(\tau - 1)/\tau + (\tau - 1)(C_2(\tau + 1)^2 + C_3) + C_4 \ln \tau))]$$

### 1.4 饱和液体比容方程

$$V' = V_{KP}/\text{EXP}[a_1(1 - \tau)^{1/3} + a_2(\tau - 1)(C_2(\tau + 1)^2 + C_3)]$$

### 1.5 汽化潜热方程

$$r = P\tau(V'' - V') [R_i/\tau + (R_i - 4 + P_s)(3C_2\tau^2 + 2C_2\tau - C_2 + C_3 + C_4/\tau + C_1/\tau^2)] \times 100$$

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### 1.6 饱和汽或过热蒸汽焓方程

$$h = T_{KP}(d_0\tau + d_1\tau^2/2 + d_2\tau^3/3 + d_3\tau^4/4 + d_4\tau^5/5) + T_{KP}R\tau^2 \times 10^{-5} [(b_2/\tau^2 + 3b_3/\tau^4)(V_0/V) + 0.5(b_5/\tau^2 + 3b_6/\tau^4)(V_0/V)^2 + 1/3(3b_7/\tau^4)(V_0/V)^3] + PV \times 10^2 + h_0$$

### 1.7 饱和液焓方程

$$h' = h'' - r$$

### 1.8 饱和汽或过热蒸汽熵方程

$$S = d_0 \ln \tau + d_1 \tau + d_2 \tau^2/2 + d_3 \tau^3/3 + d_4 \tau^4/4 + R \times 10^{-5} [\ln V \times 10^{-3} - (b_1 - 2b_3/\tau^3)(V_0/V) + (b_4 - 2b_6/\tau^3)(V_0/V)^2 - 2b_7/\tau^3(V_0/V)^3] + S_0$$

### 1.9 饱和液熵方程

$$S' = S'' - r/T$$

上述方程的有关系数见表1、表2,参数见表3。

表1 64种工质相同系数

Tab. 1 The same coefficients of sixty-four refrigerants

C <sub>1</sub>	C <sub>2</sub>	C <sub>3</sub>	C <sub>4</sub>	b <sub>1</sub>	b <sub>2</sub>	b <sub>3</sub>	b <sub>4</sub>	b <sub>5</sub>	b <sub>6</sub>	b <sub>7</sub>
4	0.2	0.5	-5.3	187.64	-475.8	-50	-7.192	53.62	-9.38	0.36

表2 64种工质不同系数

Tab. 2 The different coefficients of sixty-four refrigerants

工质种类	d <sub>0</sub>	d <sub>1</sub>	d <sub>2</sub>	d <sub>3</sub>	d <sub>4</sub>	R <sub>i</sub>	P <sub>s</sub>	a <sub>1</sub>	a <sub>2</sub>
R717	1.7262	-1.4470	2.5387	-1.2409	0.21857	7.0284	-0.3958	1.6839	0.3859
R10	0.06175	1.3804	-1.4405	0.72968	-0.14543	6.6170	0	1.5366	0.3063
R10B1	0.07438	1.1109	-1.2735	0.70685	-0.15403	6.6521	-0.1	1.4730	0.2643
R10B2	0.08175	0.96266	-1.2408	0.77196	-0.18809	6.6661	-0.1	1.4757	0.2633
R10B3	0.08630	0.78458	-1.0343	0.65569	-0.16236	6.6838	-0.1	1.4820	0.2621
R10B4	0.08915	0.71239	-1.0454	0.73461	-0.20107	6.7002	-0.1	1.3737	0.1609
R11	0.02416	1.3173	-1.1442	0.49436	-0.08504	6.5974	-0.0617	1.4617	0.2492
R11B1	0.04606	1.0570	-1.0307	0.49886	-0.09578	6.6255	-0.1	1.4749	0.2662
R11B2	0.05872	0.89579	-0.9735	0.52335	-0.11116	6.6409	-0.1	1.479	0.2651
R11B3	0.06666	0.77997	-0.9333	0.55009	-0.12754	6.659	-0.1	1.4806	0.2622
R12	-0.00515	1.1578	-0.77326	0.26424	-0.03663	6.5741	-0.0913	1.4388	0.2338
R12B1	0.02545	0.91969	-0.70713	0.27812	-0.04414	6.5956	-0.0979	1.4248	0.2179
R12B2	0.04247	0.78510	-0.69178	0.31085	-0.05600	6.6126	-0.1	1.4821	0.2670
R13	-0.02154	0.92272	-0.41891	0.09953	-0.00988	6.5553	-0.1198	1.4247	0.2255
R13B1	0.01555	0.72393	0.39540	0.11458	-0.01385	6.5392	-0.0717	1.4651	0.2581
R14	-0.01656	0.64700	-0.14916	0.0133	-0.0009	6.5595	-0.1005	1.4380	0.2240
R20	0.14913	0.64085	0.01598	-0.27996	0.9921	6.7330	-0.1	1.4700	0.2586
R20B1	0.12263	0.51829	-0.03512	-0.22128	0.09014	6.7245	-0.1	1.4761	0.2592
R20B2	0.10676	0.46417	-0.07972	-0.20012	0.09768	6.7156	-0.1	1.4787	0.2599
R20B3	0.09591	0.40779	-0.11035	-0.175	0.08494	6.7055	-0.1	1.4093	0.1869
R21	0.16113	0.52327	0.11770	-0.22460	0.05930	6.6648	0	1.4916	0.2555
R21B1	0.12657	0.43549	0.03460	-0.17227	0.05402	6.7405	-0.1	1.4784	0.2581

工质种类	$d_0$	$d_1$	$d_2$	$d_3$	$d_4$	$R_1$	$P_a$	$a_1$	$a_2$
R21B2	0.70731	0.37837	-0.02775	-0.11778	0.04324	6.7317	-0.1	1.4837	0.2587
R22	0.20428	0.31010	0.29043	-0.21960	0.04135	6.7964	-0.1644	1.4892	0.2865
R22B1	0.14885	0.26563	0.16452	-0.15762	0.03371	6.7522	-0.1	1.4837	0.2573
R23	0.3148	0.00735	0.49108	-0.22918	0.03223	6.9721	-0.2113	1.5685	0.2976
R30	0.30274	-0.17790	1.4297	-1.1312	0.27923	6.5960	-0.172	1.701	0.568
R30B1	0.19392	-0.03746	0.95765	-0.85625	0.23356	6.7351	-0.1	1.4718	0.2550
R30B2	1.4000	0.4214	0.71329	-0.73066	0.22140	6.6714	-0.1	1.4796	0.2615
R31	0.42790	-0.47547	1.4734	-0.87885	0.17098	6.8362	-0.1	1.4697	0.2514
R31B1	0.25138	-0.21159	0.92540	-0.62136	0.13413	6.8009	-0.1	1.4798	0.2539
R32	0.67743	-0.99846	1.7226	-0.78414	0.12056	7.1744	-0.5506	1.6845	0.4531
R40	0.64260	-1.0400	2.1829	-1.1920	0.22051	6.3960	0	1.4862	0.2323
R40B1	0.30512	-0.42635	1.1942	-0.74325	0.15484	6.4499	-0.1	1.7247	0.5363
R41	1.1998	-1.8387	2.2749	-0.86469	0.11471	6.7100	-0.550	1.5474	0.4853
R50	2.3702	-1.7476	1.1607	-0.23224	0.01647	5.6628	0.2106	1.9417	0.7635
R112	0.04743	1.8185	-1.9671	1.0572	-0.22438	6.9812	0	1.5293	0.2630
R113	0.02566	1.7204	-1.6121	0.76289	-0.14367	6.9168	-0.2045	1.4093	0.2074
R113B2	0.07170	1.2460	-1.3787	0.76897	-0.16997	6.8449	-0.1	1.4594	0.2269
R114	-0.00088	1.5958	-1.2584	0.50988	-0.08290	6.9220	0	1.2978	0.0305
R114B2	0.06231	1.1206	-1.0547	0.50982	-0.09840	6.8320	0	1.4680	0.2038
R115	-0.02616	1.4253	-0.90513	0.30197	-0.04103	7.0387	-0.3664	1.2431	0.0707
R116	-0.05898	1.2636	-0.62954	0.16865	-0.01874	6.8121	0	1.4093	0.1477
R142B	0.07801	1.1333	-0.29180	-0.01657	0.01477	6.9530	-0.3192	1.3500	0.0060
R143a	0.10560	0.86300	0.06359	-0.14261	0.02842	7.1818	-0.500	1.6251	0.4883
R152a	0.47035	-0.24890	1.6014	-0.90242	0.16048	6.9210	0	1.7150	0.4183
R160	0.58900	-0.85156	2.9840	-0.9308	0.40922	6.6234	0	1.4348	0.2154
R170	1.7353	-2.6785	3.5904	-1.3531	0.17616	6.2724	0.1961	1.4711	0.3390
R215	0.07239	1.82542	-1.73445	0.8448	-0.16508	7.464	-0.1650	1.0400	0.2300
R216	0.03640	1.80489	-1.5412	0.68057	-0.12079	7.212	-0.1665	1.3232	0.078
R217	0.02231	1.67027	-1.22513	0.47117	-0.07330	7.348	-0.1900	1.1940	0.0610
R218	-0.00231	1.54869	-0.96170	0.31845	-0.04312	7.2817	-0.2431	1.1986	0.0368
R290	1.07190	-1.12053	-2.04928	-0.48699	0.22695	6.4618	-0.0799	1.4603	0.2676
R3(11)0	0.94447	-0.85891	3.73867	-2.06553	0.36309	6.6834	-0.1478	1.4731	0.2861
R311(10)	-0.11539	2.05406	-1.51548	0.59282	-0.09465	7.5097	-0.2403	1.5911	0.4043
R(413)0	0.83035	0.43494	2.19173	-1.24010	0.00002	6.9421	-0.1778	1.4684	0.2830
RC318	0.07946	1.09412	-0.30106	0	0	7.3740	-0.0522	1.9834	0.7871
R1150	0.84885	-0.59999	1.39819	-0.50549	0.05901	6.1216	0	1.2566	0.0645
R1270	0.49765	0.00698	1.82944	-0.91221	0.13756	6.4663	-0.2270	1.3717	0.2442
R500	0.08481	0.96071	-0.42056	0.12288	-0.01924	6.628	0	1.4500	0.2160
R502	0.02105	1.06130	-0.55178	0.17476	-0.02568	6.7280	-0.0889	1.4749	0.2535
R503	0.43906	0.28014	0.06125	-0.04375	0.00529	6.6380	0	1.4581	0.3453
R504	0.23136	0.47383	0.08896	-0.07964	0.01117	6.8200	0	1.4569	0.2026
A1	0.52559	0.32909	0.20351	-0.16470	0.02630	7.1622	0	1.4096	0.1786

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表3 热力参数

Tab. 3 Thermodynamic parameters

工质种类	气体常数 $R \times 10$ [KJ/kg·K]	临界温度 $T_{KP}$ [K]	临界压力 $P_{KP} \times 10^{-5}$ [P <sub>a</sub> ]	临界密度 $P_{KP}$ [kg/m <sup>3</sup> ]	-40℃ $h' = 0$ $h_0$ [kJ/kg]	-40℃ $h' = 0$ $S_0$ [kJ/kg·K]
R717	4.8816	405.55	113.97	235.0	935.9067	7.471526
R10	0.5405	556.36	44.93	554.0	153.5447	0.5747318
R10B1	0.4193	602.46	46.93	696.8	131.28	0.5615435
R10B2	0.3425	668.21	48.35	793.4	126.9589	0.5988923
R10B3	0.2895	674.67	50.25	967.8	107.2717	0.5479086
R10B4	0.2507	741.99	52.13	1055.6	108.4594	0.583783
R11	0.6053	471.15	43.70	570.2	126.3288	0.3587613
R11B1	0.4573	516.26	44.40	703.9	110.3988	0.3936249
R11B2	0.3675	562.14	45.84	831.6	102.0008	0.4225789
R11B3	0.3071	605.31	47.31	954.9	95.86453	0.4410967
R12	0.6876	385.15	41.19	579.1	94.19736	0.1566644
R12B1	0.5028	426.88	42.52	741.0	84.19756	0.232509
R12B2	0.3963	472.08	43.35	866.4	79.87713	0.2856013
R13	0.7960	301.90	38.68	598.9	50.73759	-0.05506951
R13B1	0.5584	340.05	39.46	770	51.88485	0.07808733
R14	0.9448	227.55	37.45	629.7	0	0
R20	0.6965	536.6	54.72	552.4	204.6084	1.080409
R20B1	0.5075	585.43	56.05	712.2	170.3723	0.9135111
R20B2	0.3992	654.41	57.48	830.0	159.0582	0.8561309
R20B3	0.3290	684.94	59.12	988.8	138.8811	0.7585832
R21	0.8078	451.65	51.73	527.9	175.8975	0.964101
R21B1	0.5642	507.54	53.54	706.9	150.8756	0.8273588
R21B2	0.4334	543.53	54.91	880.5	128.4608	0.7115545
R22	0.9616	369.28	49.90	537.2	137.4387	0.8699267
R22B1	0.6351	411.11	51.75	750.1	113.2814	0.7005805
R23	1.1875	299.45	48.11	528.0	94.5385	0.8478446
R30	0.9789	510.00	61.70	470.0	254.9335	1.727979
R30B1	0.6426	555.49	63.22	669.2	209.2321	1.306255
R30B2	0.4783	605.70	64.69	840.5	176.0877	1.051909
R31	1.2142	424.83	60.01	443.5	251.1673	1.950345
R31B1	0.7362	468.14	61.10	637.7	180.4956	1.293861
R32	1.5982	351.55	58.43	425.1	214.6219	2.255898
R40	1.6368	416.25	64.88	399.1	283.6242	2.587971
R40.	0.8758	462.16	65.68	598.0	187.4559	1.469031
R41	2.4430	317.75	58.56	296.0	183.1907	3.082991
R50	5.1826	190.55	45.33	136.6	0	0
R112	0.4079	551.15	33.34	568.7	103.8848	0.2405297
R113	0.4437	487.15	33.89	607.6	77.4448	0.06348616
R113B2	0.3009	563.15	35.23	797	68.07073	0.2329394

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工质种类	气体常数 $R \times 10$ [KJ/kg·K]	临界温度 $T_{KP}$ [K]	临界压力 $P_{KP} \times 10^{-5}$ [P <sub>a</sub> ]	临界密度 $P_{KP}$ [kg/m <sup>3</sup> ]	-40℃ $h' = 0$ $h_0$ [kJ/kg]	-40℃ $h' = 0$ $S_0$ [kJ/kg·K]
R114	0.4864	418.85	33.33	623.0	63.87668	-0.06513775
R114B2	0.3200	487.30	33.58	812.9	53.10124	0.1352195
R115	0.5383	353.09	31.92	667.3	37.191	-0.2360268
R116	0.6024	292.85	28.83	638.1	8.378403	-0.4252721
R142B	0.8274	409.60	41.38	459.0	124.279	0.302976
R143a	0.9893	346.25	41.10	448.7	115.6431	0.4484495
R152a	1.2588	386.65	44.91	351.4	175.8328	1.396114
R160	1.2888	460.35	53.92	337.1	257.7704	2.318851
R170	2.7651	305.42	49.34	213.8	82.66835	3.528505
R215	0.3503	505.15	29.80	682.5	60.19913	0.05416495
R216	0.3763	453.14	27.49	639.1	39.4198	-0.1368734
R217	0.4066	395.15	26.90	637.1	24.29386	-0.2504943
R218	0.4422	345.05	26.77	704.5	5.364937	0.3943178
R290	1.8855	369.96	42.69	225.4	288.0335	3.483467
R3(11)0	1.4305	425.16	37.79	234.7	125.836	2.383206
R311(10)	0.3493	386.35	23.24	625.8	17.76202	-0.6006795
R(413)0	1.1524	469.77	33.89	242.6	135.7568	1.921424
RC318	0.4156	388.47	27.80	547.9	32.32735	-0.01013553
R1150	2.9637	282.65	50.56	214.0	108.3327	1.834297
R1270	1.9758	364.95	46.14	238.8	224.4923	1.767931
R500	0.8373	378.65	43.60	513.0	112.6729	0.4206838
R502	0.7448	355.31	40.10	571.7	83.53775	0.1489829
R503	0.9529	292.65	43.38	589.4	19.19545	0.4797282
R504	1.0493	339.54	47.70	531	113.2494	0.7386395
A1	0.5318	386.65	32.95	623.3	-4.836289	0.714974

表4 0℃时参数比较

Tab. 4 Thermodynamic parameters at 0℃

工质	$P_s$ [bar]	$V'$ [dm <sup>3</sup> /kg]	$V''$ [m <sup>3</sup> /kg]	$h'$ [kJ/kg]	$h''$ [kJ/kg]	$S'$ [kJ/kg·K]	$S''$ [kJ/kg·K]	数据来源
R12	3.0861	0.7159	0.055389	200.00	351.479	1.00000	1.55453	文献[1]
	3.08285	0.7166	0.05664	199.999	351.79	1.00054	1.56723	本文
R22	4.9759	0.77834	0.047135	200.00	405.364	1.000	1.75180	文献[1]
	4.97547	0.7811	0.04833	199.999	410.096	0.99999	1.76915	本文
R717	4.3017	1.56596	0.28731	121.761	1379.14	-1.43695	3.16631	文献[1]
	4.29395	1.52538	0.29823	121.774	1421.65	-1.4369	3.32193	本文

表5 270K 时参数比较

Tab. 5 Thermodynamic parameters comparison at 270k

工 质	$P_s$ [Mbar]	$\rho'$ [kg/m <sup>3</sup> ]	$V'$ [m <sup>3</sup> /kg]	$h'$ [kJ/kg]	$h''$ [kJ/kg]	$S'$ [kJ/kg·K]	$S''$ [kJ/kg·K]	数据来源
R142b	0.13046	1179.3	0.16237	33.322	246.18	0.13200	0.92036	文献[4]
	0.12973	1176.0	0.16250	33.761	247.08	0.13008	1.0001	本文
R152a	0.23860	965.27	0.13328	45.806	352.84	0.18109	1.3182	文献[4]
	0.23152	968.9	0.1334	45.159	352.36	0.18657	1.3152	本文

## 2 计算结果

根据本文给出的计算公式,用 BASIC 语言编制了计算程序[李洪芳等,1991]其计算结果与文献[沈志光等,1983]数据作比较,见表4,其结果相当一致。

在此基础上逐一调试64种工质的积分常数  $h_0$ 、 $S_0$ ,见表3。基准点为  $-40^\circ\text{C}$   $h'=0$ 、 $S'=0$ 。对 R142b、R152a 作了详细计算与文献[ASHRAE,1989]提供数据相比有较好的吻合,见表5。

## 3 结论

本文给出了64种工质的热力性质计算所需的全部公式、参考点、及参考点上的焓、焓方程的积分常数。用 BASIC 语言编制的计算程序运行结果表明计算公式正确,计算结果令人满意。为替代工质 R142b、R152a 等64种工质热力性质研究提供了条件。

## 4 符号

$P$ : 压力, Pa;  
 $T$ : 温度, K;  
 $\tau = T/T_{KP}$ : 对比温度;  
 $V$ : 比容, m<sup>3</sup>/kg;  
 $\rho$ : 密度, kg/m<sup>3</sup>;  
 $C_r$ : 定容比热, kJ/kg·K;  
 $r$ : 汽化潜热, kJ/kg;  
 $R$ : 气体常数, kJ/kg·K;  
 $h$ : 焓, kJ/kg;  
 $S$ : 熵, kJ/kg·K;  
 $h_0$ : 焓方程的积分常数;  
 $S_0$ : 熵方程的积分常数;  
 $Z = \frac{PV}{RT}$ : 压缩因子。

### 上下标

KP: 临界值;  
 $S$ : 饱和;  
 $'$ : 饱和液体;  
 $''$ : 饱和蒸汽;  
 $O$ : 理想气体。

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## COMPUTATION OF THERMODYNAMIC PROPERTIES FOR R142b, R152a, ETC. SIXTY-FOUR REFRIGERANTS

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**ABSTRACT** CFC<sub>s</sub> will be widely phased out by the end of this century. R134a and R123 are the general way to replace the refrigerants R11 and R12. Their thermodynamic properties were reported in many articles. This paper gives all basic formulas and a general calculating program presented to compute thermodynamic properties for different alternatives such as R152a、R142b, etc. The results have a good agreement with the data of existing refrigerant diagrams and charts.

**KEYWORDS** CFC<sub>s</sub>, alternates, thermodynamic properties